

BI-OBJECTIVE RELIABILITY BASED DESIGN OPTIMIZATION (RBDO) INCORPORATING STATISTICAL DATA UNCERTAINTY

Raghu R Sirimamilla, Prof. Satchi Venkataraman, San Diego State University

Objective

- The objective of this research is to develop methods to incorporate statistical data uncertainty in reliability estimation and optimization
 - -Develop methods for estimating the confidence bounds of inverse reliability measures
 - -Formulate and solve a bi-objective optimization to minimize design weight and sensitivity to data uncertainty with reliability constraints.

Introduction

- Large structural systems such as space vehicles and aerospace structures. have typical component level failure probabilities of the order of 10⁻⁴ to 10⁻⁷.
- Accurately estimating such low failure probabilities requires very high accuracy, high fidelity analyses, and accurate statistical data.
- Quantification of risk using reliability based approaches relies on availability of statistics of the random variables that affect the response.
- Uncertainty is introduced from the use of small sample sizes to estimate the distribution parameters (mean and variance - location and scale) of a chosen distribution function.
- Uncertainty in the statistical parameters and distribution functions introduces uncertainty into the reliability estimates.

Uncertainty in Failure Probability (P₄)

 Calculating probability of failure (P_i) requires evaluating the following multidimensional integral

$$P_f = \int_{g(\mathbf{x}) < 0} f_{\mathbf{x}}(\mathbf{x}) d\mathbf{x}$$

- f(x) is the joint distribution function of the random variables
- g(x) is the limit state or design constraint function
- The probability of failure due to uncertainties in design variables and distribution parameters that describe the random variables is

$$\widetilde{P}_{f} = \int_{g(\mathbf{x})<0} f_{\mathbf{x}}(\mathbf{x}) d\mathbf{x} = \int_{g(\mathbf{x})<0} \left[\int_{S_{\theta}} f_{\mathbf{x}|\theta}(\mathbf{x}|\theta) f_{\theta}(\theta) d\theta \right] d\mathbf{x}$$

- Where $f(x|\theta)$ is the condition joint probability function of random variables and $f(\theta)$ is the joint distribution function of random parameters.

Confidence Bounds for Probability of failure

- Data uncertainty is a epistemic (reducible) uncertainty resulting from insufficient information or knowledge
- . We estimate effect of statistical data uncertainty by calculating confidence bounds (interval measures) for the estimated failure probability

-An α confidence bound is given by $[(P_f)_{1-\alpha}, (P_f)_{\alpha}]$

- where
$$\begin{array}{c} (P_f)_{\alpha} : \Phi(P_{f|\theta}) = \alpha \\ (P_f)_{1-\alpha} : \Phi(P_{f|\theta}) = (1-\alpha) \end{array}$$

- The confidence bound calculated separates the effect of data (epistemic) uncertainty from variability (aleatoric uncertainty) in reliability estimation
- Estimating confidence bounds requires obtaining the cumulative distribution of failure probability







ned at the mean value

Generate values statistical narameters

(e.g. mean ($\theta_{i=1...n}$) and variance ($\sigma_{i=1...n}$)) based on their distributions (n) and calculate

e PDF at the perturbed values of distribution arameters f_v(x/0)



$$(\theta_i + \Delta \theta_i) = \frac{1}{N} \sum_{j=1}^N I_g(x) \frac{f(\mathbf{x}^{(j)} | \theta_i + \Delta \theta_i)}{f(\mathbf{x}^{(j)} | \theta_i)}$$

- urface ational effort
- · Fitting accurate response surface models for probability of failure is difficult because it changes several orders of magnitude in design space

Probability Sufficiency Factor (PSF)

- · A solution is to use and inverse reliability measure, such as Probabilistic Sufficiency Factor (PSF)
- PSF of a design is the minimum safety factor required to ensure that the any constraint violation has a probability less the specified target failure probability

Safety factor for a constraint
$$g_r(\hat{\mathbf{x}}, \mathbf{d}) \le g_c(\hat{\mathbf{x}}, \mathbf{d})$$
 is $s(\mathbf{x}, \mathbf{d}) = \frac{g_c(\hat{\mathbf{x}}, \mathbf{d})}{g_r(\hat{\mathbf{x}}, \mathbf{d})} \ge s$
Probability of failure is then defined as $P_f = \int_{s<1}^{s} f_x(\mathbf{x})$

Design reliability constraint requires $Probability(s \le 1) \le P_{z}$

An inverse measure PSF is proposed such that Probability $(s \leq P_{rf}) = P_r$

PSF is the nth smallest safety factor in a MCS

 $PSF = n^{th} \min[s_{cr}(\mathbf{x}_i)]$ $n = NP_r$

P, is the target probability of failure

Confidence Interval Calculation of PSF

- · A ratio method is proposed to calculate the PSF for perturbed values of the distribution parameters
- PSF is calculated at the distribution parameter PSF(θ) and also the perturbed value of $PSF(\theta+\Delta\theta)$, using the ratio of the joint distribution functions at MCS sampling points

$$PSF(\mathbf{\theta} + \Delta \mathbf{\theta}) = S(x^{(k)}) \qquad \text{where } S(x^{(1)}) < S(x^{(2)}) < \dots < S(x^{(p)})$$
$$k = \max(p) \qquad \text{such that} \qquad \frac{1}{N} \sum_{i=1}^{p} \frac{f(\mathbf{x}^{(i)}|\boldsymbol{\theta} + \Delta \boldsymbol{\theta})}{f(\mathbf{x}^{(1)}|\boldsymbol{\theta})} \le P_{r}$$



Variable	Mean	COV	Distribution
Load X (lb)	500	0.2	Normal
Load Y (lb)	1000	0.1	Normal
Modulus, E (psi)	29 x 10 ⁶	0.05	Normal
Strength, S (psi)	40,000	0.05	Normal
Length, L (inch)	100	0	Fixed
Max deflection, D0 (inch)	2.25	0	Fixed

Bi - Objective Function Formulation

· First Objective : Minimize volume of the cantilever beam

$$f_V = wtL$$

$$PSF_{Mean}^{Strength} \ge 1$$

 $PSF_{Mean}^{Dispalcement} \ge 1$

Second objective function: Minimize PSF confidence bound (effect of data uncertainty)

$$f_{CB} = \left(PSF_{Mean}^{Strength} - PSF_{5\%}^{Strength}\right)^2 + \left(PSF_{Mean}^{Displacement} - PSF_{5\%}^{Displacement}\right)^2$$

- Subjected to the constraints:

- Subjected to the constraints:

$$PSF_{Mean}^{Strength} \ge 1$$
$$PSF_{Mean}^{Dispalcement} \ge 1$$

- · Optimized the individual objective functions and obtained their respective values as shown in the figure below
- · Normalize the two objective functions using the optimum values obtained from single objective optimization
- Used a weighted sum approach to perform optimization for the bi-objective case

$$f = (1 - \alpha)f_V + \alpha f_{CB}$$

• Varied the weighting coefficient α from the 0 to 1 and repeated optimization to develop the pareto-optimum curve



Conclusions

- Developed methods to estimate the confidence bounds for the inverse probability measures (PSF).
- · Performed robust reliability based design optimization.

....

No of

10

100

samples Factor

Safety

0.78

0.80

0.82

0.87 0.93

0.99

1.04

2.03

2.14

0 if g(x) > 0

Sampling Based Methods (Monte Carlo Simulation)

Simulation

Probability of failure (Pt) using Monte Carlo

 $P_f = \frac{1}{N} \sum_{i=1}^{N} I_g(\mathbf{x})$

 $I_{-}(x) =$

$$(\theta_i + \Delta \theta_i) = \frac{1}{N} \sum_{j=1}^{N} I_g(x) \frac{f(\mathbf{x}^{(j)} | \theta_i + \Delta \theta_i)}{f(\mathbf{x}^{(j)} | \theta_i)}$$

Calculate the ratio, $r = f_{\chi}(x/\theta_{mean})/f_{\chi}(x/\theta_i)$ and $Pf(\theta_i) = I_s(x/\theta_{mean}) * r$

Calculate the 95th of probability f failure or 5th % of reliability index Stop